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# Thermodynamic modeling of the U-Mn and U-Nb systems

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#### ABSTRACT

The thermodynamic assessments of the U–Mn and U–Nb binary systems were carried out by using the CALPHAD (Calculation of Phase Diagrams) method incorporating experimental thermodynamic properties and phase equilibria. The Gibbs free energies of the liquid, bcc, fcc,  $\alpha U$  and  $\beta U$  phases were described by the subregular solution model with the Redlich–Kister equation, and those of the intermetallic compounds (Mn<sub>2</sub>U and MnU<sub>6</sub>) in the U–Mn binary system were described by the two-sublattice model. The thermodynamic parameters of the U–Mn and U–Nb binary systems were optimized to reproduce the experimental data, and provide agreement with the experimentally determined phase diagram for each binary system.

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#### 1. Introduction

The use of uranium in the production of energy from nuclear fission has given considerable impetus to the investigation of the U alloys in recent decades. The investigations of U-based alloys focus not only on the U compounds used in the fuels, but also on the alloys of U and common elements of the structural materials and fission products [1–3]. Mn and Nb are very important alloying elements for the U-based alloys [4–9]. In order to develop new nuclear materials, it is necessary to understand the phase equilibria in U-based alloy systems.

The CALPHAD method is a powerful tool to reduce cost and time during development of materials [10]. As a result, it is of great importance to establish the thermodynamic database for the Ubased alloys system. In this paper, as a part of thermodynamic database of U-based alloy systems, the thermodynamic descriptions for the phase equilibria in the U–Mn and U–Nb systems were carried out by means of the CALPHAD method.

### 2. Thermodynamic model

The information of stable solid phases and the used models in the U–Mn and the U–Nb systems [11] is listed in Table 1.

#### 2.1. Solution phases

The Gibbs free energies of the solution phases in Me–U (Me: Mn, Nb) system were described by the subregular solution model

[12]. The molar Gibbs free energy of each solution phase in the Me–U system is given as follows:

$$G^{\phi} = x_{Me}^{0} G_{Me}^{\phi} + x_{U}^{0} G_{U}^{\phi} + RT(x_{Me} \ln x_{Me} + x_{U} \ln x_{U}) + x_{Me} x_{U} \sum_{m=0}^{n} L_{Me,U}^{\phi} (x_{Me} - x_{U})^{m},$$
(1)

where  ${}^{0}G_{Me}^{\phi}$  and  ${}^{0}G_{U}^{\phi}$  are the molar Gibbs free energy of pure element Me and U with the structure  $\phi$  in a nonmagnetic state, which is taken from the compilation by Dinsdale [13] and shown in Table 2. The  $x_{Me}$  and  $x_{U}$  are the mole fractions of Me and U components, and  ${}^{m}L_{Me,U}^{\phi}$  is the interaction energy between Me and U atoms, and expressed as:

$${}^{m}L^{\phi}_{\mathrm{Me},\mathrm{U}} = a + bT + cT\ln(T), \tag{2}$$

the parameters of a, b and c are evaluated based on the experimental data in the present work.

#### 2.2. Stoichiometric intermetallic compounds

The  $Mn_2U$  and  $MnU_6$  compounds in the U–Mn system are treated as stoichiometric phases. The Gibbs free energy of formation per mole of formula unit  $(Mn)_m(U)_n$  can be expressed by the two-sublattice model [14], as the following equation referring to the pure elements in their nonmagnetic state:

$$\Delta G_{f}^{\mathrm{Mn}_{m}\mathrm{U}_{n}} = {}^{0}G_{f}^{\mathrm{Mn}_{m}\mathrm{U}_{n}} - m^{0}G_{\mathrm{Mn}}^{\mathrm{ref}} - n^{0}G_{\mathrm{U}}^{\mathrm{ref}} = a' + b'T, \qquad (3)$$

where the  $\Delta G_f^{Mn_m U_n}$  denotes the standard Gibbs free energy of formation of the stoichiometric compound from the pure elements.



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## Table 1

The stable solid phases and the models used in the U-Mn and U-Nb systems

System	Phase	Prototype	Struckturbericht designation	Modeling phase	Used models
U–Mn	δMn	W	A2	(U,Mn)	Subregular solution model
	γMn	Cu	A1	(U,Mn)	Subregular solution model
	βMn	βMn	A13	(U,Mn)	Subregular solution model
	αMn	αMn	A12	(Mn)	Subregular solution model
	Mn <sub>2</sub> U	$Cu_2Mg$	C15	$(Mn)_2(U)$	Two-sublattice model
	MnU <sub>6</sub>	MnU <sub>6</sub>	D2 <sub>c</sub>	$(Mn)(U)_6$	Two-sublattice model
	γU	W	A2	(U,Mn)	Subregular solution model
	βU	βU	A <sub>b</sub>	(U,Mn)	Subregular solution model
	αU	ά	A20	(U)	Subregular solution model
U–Nb	(yU,Nb)	W	A2	(U,Nb)	Subregular solution model
	βU	βU	Ab	(U,Nb)	Subregular solution model
	αU	αU	A20	(U,Nb)	Subregular solution model

## Table 2

Gibbs energy parameters of condensed pure elements [13]

Gibbs free energy (J/mol)	Temperature (K)
Liquid phase $G_{U}^{SER}$ +3947.766 + 120.631251 T - 26.9182 Tln(T) + 1.25156 × 10 <sup>-3</sup> T <sup>2</sup> - 4.42605 × 10 <sup>-6</sup> T <sup>3</sup> + 38568 T <sup>-1</sup> -10166.3 + 281.797193 T - 48.66 Tln(T)	298.15 < T < 955 955 < T < 3000
$G_{Mn}^{SER}$ +9744.63 + 117.4382 <i>T</i> - 23.4582 <i>T</i> ln( <i>T</i> ) - 7.34768 × 10 <sup>-3</sup> <i>T</i> <sup>2</sup> + 69827 <i>T</i> <sup>-1</sup> - 4.41929 × 10 <sup>-21</sup> <i>T</i> <sup>7</sup> - 9993.9 + 299.036 <i>T</i> - 48 <i>T</i> ln( <i>T</i> )	298.15 < <i>T</i> < 1519 1519 < <i>T</i> < 2000
$ \begin{array}{l} G_{\text{Nb}}^{\text{SR}} \\ +21262.202 + 131.229057 \ \text{T} - 26.4711 \ \text{Th}(\text{T}) + 2.03475 \times 10^{-4} \ \text{T}^2 - 3.5012 \times 10^{-7} \ \text{T}^3 + 93399 \ \text{T}^{-1} - 3.06098 \times 10^{-23} \ \text{T}^7 \\ - 7499.398 + 260.756148 \ \text{T} - 41.77 \ \text{Th}(\text{T}) \end{array} $	298.15 < <i>T</i> < 2750 2750 < <i>T</i> < 6000
a Mn phase $G_{Mn}^{SER}$ -8115.28 + 130.059 T - 23.4582 Tln(T) - 7.34768 × 10 <sup>-3</sup> T <sup>2</sup> + 69.827 T <sup>-1</sup> -28733.41 + 312.2648 T - 48 Tln(T) + 1.656848 × 1030 T <sup>-9</sup>	298.15 < T < 1519 1519 < T < 2000
	298.15 < T < 1519 1519 < T < 2000
$\alpha U$ phase $G_{U}^{SUR}$ = -8407.734 + 130.955151 T - 26.9182 Tln(T) + 1.25156 $\times$ 10 <sup>-3</sup> T <sup>2</sup> - 4.42605 $\times$ 10 <sup>-6</sup> T <sup>3</sup> + 38568 T <sup>-1</sup> = -22521.8 + 292.121093 T - 48.66 Tln(T)	298.15 < T < 955 955 < T < 3000
βU phase $G_U^{SER}$ -5156.136 + 106.976316 T - 22.841 Tln(T) - 1.084475 × 10 <sup>-2</sup> T <sup>2</sup> + 2.7889 × 10 <sup>-8</sup> T <sup>3</sup> + 81944 T <sup>-1</sup> -14327.309 + 244.16802 T - 42.9278 Tln(T)	298.15 < <i>T</i> < 941.5 941.5 < <i>T</i> < 3000
Bcc_A2 phase $G_{U}^{SER}$ -752.767 + 131.5381 T - 27.5152 Tln(T) - 8.35595 × 10 <sup>-3</sup> T <sup>2</sup> + 9.67907 × 10 <sup>-7</sup> T <sup>3</sup> + 204611 T <sup>-1</sup> -4698.365 + 202.685635 T - 38.2836 Tln(T) $G_{Mn}^{SER}$ -3235 3 + 127 85 T - 23 7 Tln(T) - 7.44271 × 10 <sup>-3</sup> T <sup>2</sup> + 60000 T <sup>-1</sup>	298.15 < <i>T</i> < 1049 1049 < <i>T</i> < 3000 298.15 < <i>T</i> < 1519
$ \begin{array}{l} -23183 + 307.7043 \ T - 48 \ Tln(T) + 1.265153 \times 1030 \ T^{-9} \\ G_{ND}^{SER} \\ -8519.353 + 142.045475 \ T - 26.4711 \ Tln(T) + 2.03475 \times 10^{-4} \ T^2 - 3.5012 \times 10^{-7} \ T^3 + 93 \ 399 \ T^{-1} \\ -37669.3 + 271.720843 \ T - 41.77 \ Tln(T) + 1.528239 \times 1032 \ T^{-9} \end{array} $	298.15 < T < 2750 2750 < T < 6000
Fcc_A1 phase $G_{\rm U}^{\rm SER}$ -3407.734 + 130.955151 T - 26.9182 Tln(T) + 1.25156 × 10 <sup>-3</sup> T <sup>2</sup> - 4.42605 × 10 <sup>-6</sup> T <sup>-3</sup> + 38568 T <sup>-1</sup> - 17521.8 + 292.121093 T - 48.66 Tln(T)	298.15 < T < 955 955 < T < 3000
$ \begin{array}{l} G_{\rm Mn}^{\rm SER} \\ -3439.3 + 131.884 \ T - 24.5177 \ Tln(T) - 0.006 \ T^2 + 69600 \ T^{-1} \\ -26070.1 + 309.6664 \ T - 48 \ Tln(T) + 3.86196 \times 1030 \ T^{-9} \end{array} $	298.15 < <i>T</i> < 1519 1519 < <i>T</i> < 2000

The terms  ${}^{0}G_{Mn}^{ref}$  and  ${}^{0}G_{U}^{ref}$  are the molar Gibbs free energy of pure element Mn and U with its defined reference structure in a nonmag-

netic state. The parameters of a' and b' are evaluated in the present optimization.



Fig. 1. The phase diagram of the U-Mn system reviewed by Massalski et al. [17].

## 3. Experimental information

#### 3.1. The U-Mn system

The phase diagram of the U–Mn system consists of seven solution phases ( $\alpha$ Mn,  $\beta$ Mn,  $\gamma$ Mn,  $\delta$ Mn,  $\alpha$ U,  $\beta$ U,  $\gamma$ U), and two intermetallic compounds (MnU<sub>6</sub> and Mn<sub>2</sub>U phases). The phase diagram in the U–Mn system was originally proposed by Wilhelm and Carlson [15], and then reassessed by Hanse et al. [16] and Massalski [17]. The maximum solubility of Mn in the  $\gamma$ U phase was estimated to be less than 1 wt% based on metallography. Although the solubilities of U in all the allotropes of Mn have not been investigated thoroughly, some solid solubilities were found by Whilhelm using X-ray studies [15]. The Mn<sub>2</sub>U phase has three polymorphs:  $\alpha$ Mn<sub>2</sub>U,  $\beta$ Mn<sub>2</sub>U and  $\gamma$ Mn<sub>2</sub>U. The polymorphic transformation temperatures of the  $\gamma$ Mn<sub>2</sub>U  $\leftrightarrow \beta$ Mn<sub>2</sub>U and  $\beta$ Mn<sub>2</sub>U  $\leftrightarrow \alpha$ Mn<sub>2</sub>U were respectively reported to be –61 °C and –161 °C [17]. Because these transformation



Fig. 2. The phase diagram of the U–Nb system reviewed by Koike et al. [31].

tion temperatures of the  $Mn_2U$  phase were too low to use in the present assessment, the  $Mn_2U$  phase is treated as one stoichiometric phase. The phase diagram of the U–Mn system reviewed by Massalski [17] is shown in Fig. 1.

In addition, the enthalpies and entropies of formation of the compounds ( $MnU_6$  and  $Mn_2U$ ) in the temperature range from 660 °C to 860 °C were determined by Lebedev et al. [18] on the basis of Electromagnetic Fields (EMF) measurements.

#### 3.2. The U–Nb system

The U–Nb system consists of three solution phases ( $\alpha U$ ,  $\beta U$  and ( $\gamma U$ , Nb)), and a phase separation ( $\gamma U + (Nb)$ ) in the bcc phase at lower temperature. The phase diagram in the U–Nb system has been investigated by many researchers [16,19–31]. There are two different conclusions for the monotectoid reaction of  $\gamma U$  in this system as follows: the reaction of  $\gamma U \leftrightarrow (Nb) + \alpha U$  was reported



Fig. 3. Calculated phase diagram of U-Mn binary system with experimental data [15,17].

by Roger et al. [16,22,25,28], and the  $\gamma U \leftrightarrow (Nb) + \beta U$  was reported by Terekhov [29]. Massalski [17] reviewed the phase diagram according to Rogers [22] and Terekhov [29], where the monotectoid reaction of the  $\gamma U \leftrightarrow (Nb) + \beta U$  is accepted [29]. However, in the Koike review [31], the monotectoid reaction of the  $\gamma U \leftrightarrow N$  $b + \alpha U$  is adopted according to the previous work [16,17,19– 28,30]. The liquidus line was only estimated by Rogers [22], because of the difficulty in the experiment. In this work, the assessment was carried out on the basis of the experiment data by [17,21–23,30], and the monotectoid reaction of the  $\gamma U \leftrightarrow (N-b) + \alpha U$  was adopted. The phase diagram reviewed by Koike, et al. [31] is shown in Fig. 2.

In addition, the physical properties such as the Debye temperature and Young's modulus of the solid solution alloys were determined based on the fused salt EMF measurements by Fedorov and Smirnov [32] and by Vamberskij et al. [33]. Vamberskij et al.



**Fig. 4.** Calculated enthalpies of formation of intermetallic compounds at 677 °C in the U–Mn system compared with the experimental data [18]: the reference states are  $\gamma$ U phase and  $\beta$ Mn phase.



**Fig. 5.** Calculated entropies of formation intermetallic compounds at 677 °C in the U–Mn system compared with the experimental data [18]: the reference states are  $\gamma$ U phase and  $\beta$ Mn phase.

[33] also calculated Gibbs free energies of formation of the U–Nb system at 775 °C and 900 °C by the Gibbs–Duhem equations according to their experimental data.

### 4. Optimized results and discussion

Optimization of thermodynamic parameters describing the Gibbs free energies of each phase is carried out using PARROT [34] module in the Thermo-Calc software [35], a computer program that can accept different types of data, such as any specific thermodynamic quantities and phase equilibria, in the same operation. Each piece of the selected data is given a certain weight and

#### Table 3

Thermodynamic parameters for the U-Mn system optimized in this work

Parameters in each phase (J/mol)
Liquid phase, format $(Mn,U)_1$ ${}^0L^{iq}_{Mn,U} = -23400 + 11.7T$ ${}^1L^{iq}_{Mn,u} = 320 - 1.77T$
$^{\text{Min},\text{U}}_{\text{Mn},\text{U}} = -10966 + 10.4T$
$\begin{array}{l} A2 \; (\gamma U, \delta Mn) \; phase, \; format \; (Mn, U)_1 (Va)_3 \\ {}^{0}L_{Mn, U}^{bcc} \; = \; 11\; 000 + 9.83T \\ {}^{1}L_{Mn, U}^{bcc} \; = \; 2800 + 4.7T \end{array}$
$ \begin{array}{l} A_b \ \beta U \ phase, \ format \ (Mn,U)_1 \\ G_{Mn}^{\beta U} = G_{Mn}^{2Mn} + 25000 \\ 0 L_{Mn,U}^{\beta U} = 29614.8 - 12.5T \\ 1 L_{Mn,U}^{\beta U} = 69425 - 48.7T \\ 2 L_{Mn,U}^{\beta U} = -49519.7 + 47.07T \end{array} $
A1 $\gamma$ Mn phase, format (Mn,U) <sub>1</sub> (Va) <sub>1</sub> ${}^{0}L_{Mn,U}^{fcc} = 25000$
A13 $\beta Mn$ phase, format $(Mn,U)_{1}(Va)_{1}$ $G_{U}^{\beta(Mn)} = G_{U}^{\alpha U} + 5000$ ${}^{\beta Mn}_{Mn,U} = 7971 + 6.97T$
$\begin{array}{l} Mn_2 U \ phase, \ format \ (Mn)_{0.6667} \ (U)_{0.3333} \\ G^{Mn_2 U}_{Mn:U} = 0.6667 G^{zMn}_{Mn} + \ 0.3333 G^{zU}_U - 9100 - 0.32T \end{array}$
$\begin{array}{l} MnU_6 \ phase, \ format \ (Mn)_{0.1429} \ (U)_{0.8571} \\ M^{MU_6}_{Mnull} = \ 0.1429G^{Mn}_{Mn} + 0.8571G^{U}_{7U} - 5090 + 2.71T \end{array}$



Fig. 6. Calculated phase diagram of U-Nb binary system with experimental data [17,21-23,30].

#### Table 4

A comparison of calculated invariant reactions and special points in the U-Mn system with experimental results

Reaction type	Reaction	Mn (a	ıt.%)		T (°C)	References
Catatectic	$\gamma U \rightarrow \beta U + L$	2.3	1.2	20.6	745	[17]
		2.7	1.22	19.3	745	[This work]
Peritectic	$\beta U + L \rightarrow MnU_6$	1.2	21.5	14.3	725	[17]
		1.3	21	14.3	725	[This work]
Eutectoid	$\beta U \rightarrow \alpha U + MnU_6$	1.2	0	14.3	626	[17]
Eutectic	$L \rightarrow MnU_6 + Mn_2U$	21.5	14.3	66.7	716	[17]
		22.6	14.3	66.7	716	[This work]
Eutectic	$L \rightarrow \beta Mn + Mn_2U$	84	-	66.7	1035	[17]
		83.7	98.9	66.7	1035	[This work]
Melting	$L \rightarrow Mn_2U$		66.7		1120	[17]
			66.7		1120	[This work]
Peritectic	$\delta Mn + L \rightarrow \gamma Mn$	-	-	-	-	_
		99.7	92.5	99.8	1142	[This work]
Peritectic	$\gamma Mn + L \rightarrow \beta Mn$	-	-	-	-	_
		99.6	90.1	99.3	1111	[This work]
Eutectoid	$\beta Mn \rightarrow \alpha Mn + Mn_2 U$	-	-	-	-	_
		99.7	1	66.7	698	[This work]

the weight can be changed until a satisfactory description for most of the selected data is achieved.

#### 4.1. The U-Mn system

The calculated phase diagram of the U–Mn system compared to all the experimental data [15,17] used in the present optimization is shown in Fig. 3. It is seen from Fig. 3 that the calculated results are in agreement with Massalski [17], but there are some differences with Wilhelm [15] in the Mn-rich region. The calculated largest solid solubilities of U in the  $\beta$ Mn,  $\gamma$ Mn and  $\delta$ Mn phases are respectively 0.7 at.%, 0.4 at.% and 0.3 at.%. In the Mn-rich region, a little solubility of U in the  $\beta$ Mn and  $\gamma$ Mn was given in this work, although there are no experimental data about this point. The calculated enthalpies and entropies of formation of the compounds with the experimental data at 677 °C are shown in Figs. 4 and 5. The calculated results are in good agreement with the experimental data [18].

A complete set of the thermodynamic parameters describing the Gibbs free energy of each phase, including the elements as well,



Fig. 7. Calculated phase diagram of U–Nb binary system in the U-rich portion with experimental data [21,22,30].

#### 4.2. The U–Nb system

The calculated U–Nb phase diagram with the experimental data is shown in Figs. 6 and 7. The calculated phase diagram, especially the phase boundary of miscibility gap region ( $\gamma$ U + Nb), is in agreement with the experimental data [17,21–23,30]. The calculated liquidus line agrees with Rogers [22] and the Massalski review [17]. Figs. 8 and 9, respectively indicate the calculated Gibbs free energies at 775 °C and 900 °C compared with the data obtained from the Gibbs–Duhem equations [33]. It is seen from Figs. 8 and 9 that there are some differences between the present calculated results and data reported by Vamberskij [33]. In particular, in the



**Fig. 8.** Calculated Gibbs free energy at 775 °C in the U–Nb system compared with the calculation data by Vamberskij et al. [33]: the reference states are bcc  $\gamma$ U phase and bcc (Nb) phase.

Table 5	;
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Thermodynamic parameters for the U-Nb system optimized in this work

Parameters in each phase (J/mol)
Liquid phase, format (Nb,U)1
${}^{0}L_{\rm Nb,U}^{\rm Liq} = 39836.8 - 41.2T$
${}^{1}L_{\rm Nb,U}^{\rm Liq} = -149230.3 + 47.2T + 4.66T\ln(T)$
${}^{2}L_{\rm Nb,U}^{\rm Liq} = -38091.3 - 4.33T$
A2 ( $\gamma$ U,Nb) phase, format (Nb,U) <sub>1</sub> (Va) <sub>3</sub>
${}^{0}L_{\rm Nb,U}^{\rm bcc} = 17706.2 - 23.099T$
$^{1}L_{\rm Nb,U}^{\rm bcc} = -54699.5 + 30.02T$
$^{2}L_{\rm Nb,U}^{\rm bcc} = -42938.27 + 9.6T$
${}^{3}L_{\rm Nb,U}^{\rm bcc} = -28942 + 11.06T$
$A_b \beta U$ phase, format $(Nb,U)_1$
$G_{\rm Nb}^{\beta \rm U} = G_{\rm Nb}^{\rm bcc} + 15000$
${}^{0}L_{\rm Nb,U}^{eta U}=4018.4$
A20 $\alpha$ U phase, format (Nb,U) <sub>1</sub>
$G_{\rm Nb}^{\alpha \rm U} = G_{\rm Nb}^{\rm bcc} + 25000$
$^{0}L_{\mathrm{Nb},\mathrm{U}}^{\mathrm{zU}}=-5000$

#### Table 6

A comparison of calculated invariant	reactions and special points in the	U-Nb system with experime	ntal results
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Reaction type	Reaction	Nb (at.%)			T (°C)	References
Eutectoid	$\beta U \rightarrow \alpha U + \gamma U$	1.3	0.5-0.9	10.5~11.5	664	[31]
		1.3	1.09	10.1	664	[This work]
Monotectoid	$\gamma U \rightarrow \alpha U + (Nb)$	13.3	0.5	68~72	647	[31]
		13.9	1.3	70	647	[This work]
Critical	$(\gamma U, Nb) \rightarrow \gamma U + (Nb)$		52.3		930-970	[31]
			50.7		958	[This work]



Fig. 9. Calculated Gibbs free energy at 900 °C in the U-Nb system compared with the calculation data by Vamberskij et al. [33]: the reference states are bcc  $\gamma$ U phase and bcc (Nb) phase.

 $\gamma$ U + (Nb) miscibility gap region, the calculated Gibbs free energies are higher than ones by Vamberskij. However, the present calculations are reasonable by considering the error range of Vamberskij's data

A complete set of the thermodynamic parameters describing the Gibbs free energy of each phase in this system is given in Table 5, and all invariant reactions in the U-Nb system are summarized in Table 6, in which the experimental data are also listed for comparison [31].

#### 5. Conclusions

The phase diagrams and thermodynamic properties in the U-Mn and U-Nb binary systems were evaluated by combining the thermodynamic models with the available experimental information in literature. A consistent set of optimized thermodynamic parameters has been derived for describing the Gibbs free energy of each solution phase and intermetallic compounds in the U-Mn and U-Nb binary systems. Good agreement between the calculated results and most of the experimental data is obtained.

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#### References

- [1] C. Guéneau, S. Chatain, S. Gossé, C. Rado, O. Rapaud, J. Lechelle, J.C. Dumas, C. Chatillon, J. Nucl. Mater. 344 (2005) 191.
- R. Schmid-Fetzer, D. Andersson, P.Y. Chevalier, L. Eleno, O. Fabrichnaya, U.R. Kattner, B. Sundman, C. Wang, A. Watson, L. Zabdyr, M. Zinkevich, Comput. Coupling Phase Diagr. Thermochem. 31 (2007) 38.
- C. Degueldre, C. Guéneau, J. Nucl. Mater. 352 (2006) ix.
- R. Jerlerud Pérez, A.R. Massih, J. Nucl. Mater. 360 (2007) 242.
- C. Ramos, C. Saragovi, M.S. Granovsky, J. Nucl. Mater. 366 (2007) 198. [5]
- GM. Ludtka, Metall. Trans. 24A (1993) 379.
- Ì7Ì V.K. Shamardin, T.M. Bulanova, V.N. Golovanov, V.S. Neustroyev, A.V. Povstyanko, Z.E. Ostrovsky, J. Nucl. Mater. 233–237 (1996) 162.
- Y. Suzuki, T. Saida, F. Kudough, J. Nucl. Mater. 258-263 (1998) 1687.
- E.T. Cheng, G. Saji, J. Nucl. Mater. 212-215 (1994) 621.
- [10] L. Kaufman, H. Bernstein, Computer Calculation of Phase Diagram, Academic Press, New York, 1970.
- [11] H. Okamoto, Desk Handbook-Phase Diagrams for Binary Alloys, ASM International, 2000.
- [12] H.K. Hardy, Acta Metall. (1) (1953) 202;
- H.K. Hardy, Acta Metall. (2) (1954) 348. [13] A.T. Dinsdale, CALPHAD 15 (1991) 317.
- [14]
- M. Hillert, L.I. Stafansson, Acta. Chem. Scand. 24 (1970) 3618. [15] H.A. Wilhelm, O.N. Carlson, Trans. ASM 42 (1950) 1311.
- [16] M. Hansen, K. Anderko, Constitution of Binary Alloys, McGraw-Hill, New York or General Electric Co., Business Growth Services, Schenectady, New York, 1958
- [17] T.B. Massalski, P.R. Subramanian, H. Okamoto, L. Kacprzak, ASM Int. 1990.
- [18] V.A. Lebedev, V.I. Lyazgin, A.V. Ishutin, I.F. Nichkov, S.P. Raspopin, Russ. Metall. 2 (1973) 160.
- [19] H.A. Saller, E.A. Rough, US Atom. Energy Comm. BMI-1000 (1955) 48.
- [20] A.E. Dwight, M.H. Mueller, US Atom. Energy Comm. ANL-5581(1957).
- [21] P.C.L. Pfeil, J.D. Browne, G.K. Williamson, J. Inst. Metals. 87 (1958) 204.
- [22] B.A. Rogers, D.F. Atkins, E.J. Manthos, M.E. Kirkpatrick, Trans. Metall. Soc. AIME 212 (1958) 387.
- [23] O.S. Ivanov, G.I. Terekhov, US Atom. Energy Comm. 18-32 (1961).
- [24] A.D. Roming, Sandia Rep. SAND-86-0906C, Albuquerque, NM (1986)
- [25] R.P. Elliott, Constitution of Binary Alloys, First Supplement, McGraw-Hill, New York, 1965.
- [26] F.A. Shunk, Constitution of Binary Alloys, Second Supplement, McGraw-Hill, New York, 1969.
- [27] P. Feschotte, D.T. Livey, O. von Goldbeck, Atomic Energy Review, Special Issue No. 2, IAEA, Vienna (1968), 45.
- [28] P. Chiotti, V.V. Akhachinskij, I. Ansara, The Chemical Thermodynamics of Actinide Elements and Compounds, Part 5: The Actinide Binary Alloys, in: V. Medvedev, M.H. Rand, E.F. Westrum Jr., F.L. Oetting (Eds.), International Atomic Energy Agency, Vienna, 1981
- [29] G.I. Terekhov, Russ. Metall. 4 (1982) 170.
- [30] C. Fizzotti, A. Maspereni, Com. Naz. Energ. Nucl. RTIMET(66)-1 (1966) 1.
- [31] J. Koike, M.E. Kassner, R.E. Tate, R.S. Rosen, Phase Diagrams of Binary Actinide Alloys, in: M.E. Kassner, D.E. Peterson (Eds.), ASM International, Materials Park, OH, 1995.
- G.B. Fedorov, E.A. Smirnov, Sov. J. Atom. Energy. 21 (1966) 837 [32]
- Y.V. Vamberskij, A.L. Udovskij, O.S. Ivanov, J. Nucl. Mater. 55 (1975) 96. [33]
- B. Jansson, Ph.D. Thesis, Division of Physical Metallurgy, Royal Institute of [34] Technology, Stockholm, Sweden, 1984.
- [35] B. Sundman, B. Jansson, J.O. Andersson, CALPHAD 9 (1985) 153.